Using the Reactance Chart for Filter Design Problems

H. B. DAVIS*

Calculations of components for various filter and equalizer circuits are simplified by graphical means.

THE VALUE OF the reactance chart such as that shown in Fig. 1 is becoming more and more widely recognized as time goes on. Although it was originally indicated by Slon-czewsky that the chart could be used for other purposes than reactance and resonant-frequency calculations, it is still largely used for that purpose. The other short-cuts offered by the chart have been largely neglected.

It has been known for some time that these charts could be used for certain filter calculations. It is the purpose of this article to show why this is true and how it may be done for several popular types of filters. Although the material may not be new to many readers, it is felt that there are others to whom the information may be of value.

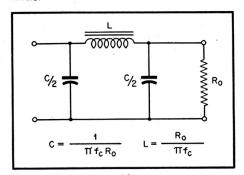


Fig. 2. Low-pass filter prototype, or constant-k section. $R \circ$ is the terminating resistance; $f \circ$ is cut-off frequency.

The chart is designed to solve equations of three parameters in which 2π enters as a factor. Specifically it solves such equations as

$$X_L = 2\pi f L \tag{1}$$

$$X_c = \frac{1}{2\pi fC} \tag{2}$$

$$f = \frac{1}{2\pi\sqrt{LC}} \tag{3}$$

Solving for L and C in equations (1) and (2) gives

$$L = \frac{X_L}{2\pi f} \tag{4}$$

$$C = \frac{1}{2\pi f X_c} \tag{5}$$

The chart may be used to solve these or other three-parameter equations having 2π as a factor if the equation to be solved can be put into one of these or an equivalent form.

Inductive and capacitive reactance have the dimensions of resistance. Therefore, without changing the form of the equations of the ordinate of the chart equations, (1) and (2) may be written

$$R_{i} = 2\pi f L \tag{6}$$

$$R_{t} = \frac{1}{2\pi fC} \tag{7}$$

Solving equations (6) and (7) for L and C respectively gives

$$L = \frac{R_i}{2\pi f} = \frac{1}{2} \cdot \frac{R_i}{\pi f} \tag{8}$$

$$C = \frac{1}{2\pi f R_z} = \frac{1}{2} \cdot \frac{1}{\pi f R_z} \qquad (9)$$

Equations (8) and (9) are seen to be very similar to the equations for the low-pass filter prototype shown in Fig. 2. The equations indicate, however, that the values given by the reactance chart for L and C will be equal to one half of the value calculated from the prototype equations if R_0 is substituted for R_1 and R_2 and f_0 is substituted for f.

For example, if it is desired to design a 10,000-ohm filter section with a cut-off frequency f_c of 1,000 cps, substituting these values in the equations of Fig. 2 give

$$L = \frac{10,000}{\pi \times 1000} = 3.18H$$
, and

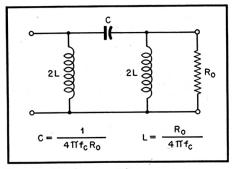


Fig. 3. High-pass filter prototype, or constant-k section.

$$C = \frac{1}{\pi \times 1000 \times 10,000} = 0.0318 \ \mu f$$

Using the reactance chart and entering the chart at $R_0=10,000\Omega$ at the intersection with the 1000 cps vertical, it

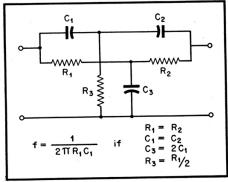
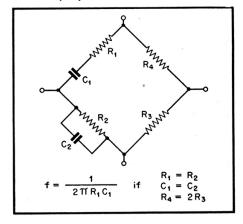


Fig. 4 (above). Parallel-T rejection or null network configuration.

Fig. 5. (below). Wien bridge circuit as employed in RC oscillators.



is found that L is given as 1.59 Henrys and C is 0.0159 μ f. These values are exactly half of the values found from the equations.

In a similar manner, if f_{\circ} is substituted for f and R_{\circ} for X_{\perp} and X_{\circ} in equations (4) and (5), equations (10) and (11) result.

$$L = \frac{R_o}{2\pi f_c} \tag{10}$$

$$C = \frac{1}{2\pi f_c R_o} \tag{11}$$

These equations are seen to be simi-

^{*7721} Old Georgetown Rd., Bethesda 14, Md.

iar to the high-pass prototype equations shown in Fig. 3. Dividing both sides of equations (10) and (11) by two yields

$$\frac{L}{2} = \frac{R_o}{4\pi f_c}$$

$$\frac{C}{2} = \frac{1}{4\pi f_c R_o}$$

Solving these equations for L and C

$$L=2 imesrac{R_o}{4\pi f_c}$$

$$C = 2 \times \frac{1}{4\pi f_c R_o}$$

From these equations it is seen that the values of L and C obtained from the reactance chart will be exactly twice the value obtained from the high-pass filter prototype equations. That this is true may be verified by solving the equations for the filters and comparing the results with the values obtained from the chart.

If equation (2) is solved for f and [Continued on page 40]

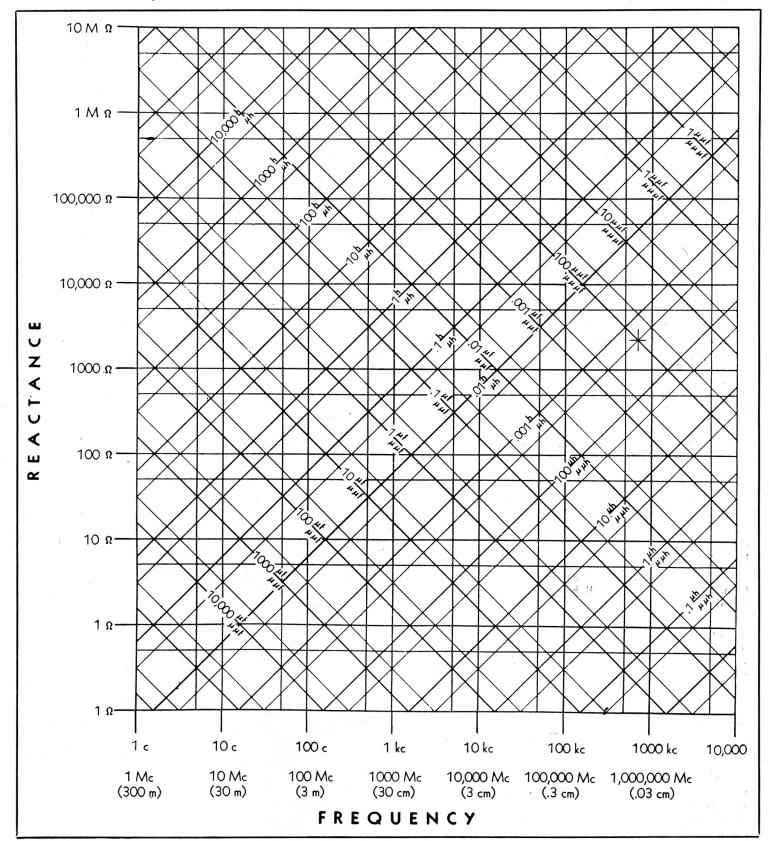


Fig. 1. The reactance chart, well known for its many applications in circuit calculations.

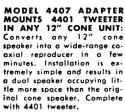
(Courtesy General Radio Company)



WIDEST SELECTION • BEST VALUE • HIGHEST QUALITY

SINGLE UNIT TWEETERS

MODELS 4408, 4409—600 CYCLE TWEETERS: Recommended for highest quality reproduction systems requiring a low crossover frequency. Cobra shaped horn results in perfect wide angle distribution. Frequency response 600 to 15,000 cycles. Model 4408 handles 6 watts and 4409 25 watts.



MODEL 4401—2000 CYCLE TWEETER: An economical 6 watt unit for converting any good 10·15" cone speaker for extended response to 15,000 cycles. Wide Angle horn, compact design and low price bring excellent high fidelity well within the popular price range.



DUAL TWEETERS



MODEL 4402, MODEL 4404: Model 4402 reproduces to 15,000 cycles. Crossover at 2000 cps. Horizontal dispersion 100°, Vertical 50°. Handles 12 watts. Compact design mounts in any radio, phono, or speaker cabinet. Model 4404 incorporates 4402 tweeter in handsome walnut cabinet complete with high-pass filter and high frequency volume control. Anyone can install.

CROSSOVER NETWORKS



MODEL 4405 HIGH PASS FILTER: An effective and economical unit for preventing lows reaching the tweeter unit. Contains high frequency control to balance highs and lows. Cutoff frequency 2000 cycles.

MODEL 4410, 4420 LC CROSSOVER NETWORK: Genuine LC frequency dividers for segregating highs and lows. Not to be confused with ordinary high-pass filters. Crossover frequencies: Model 4410 600 cycles, Model 4420 2000 cycles. Attenuator controls included and wired.

Write for Illustrated Catalog Today

— Address Inquiries to Department B



the cosine of these phase shift angles. In some cases this may cause instability of the amplifier, particularly where large amounts of feedback are used. Experience has shown that the phase shift begins to be measureable at values 1/7th to 1/10th of the frequency at which the 2 db point shows up on a gain-frequency characteristic. Therefore, the designed bandwidth should be from 7 to 10 times the highest frequency for which it is desired to have distortion less than 1 per cent. The figure shows that the phase shift through the amplifier is substantially zero from 30 to 30,000 cps.

The circuit here described in part appears to open new fields of use or improvement in present fields permiting operation very near the theoretical maximum efficiency and yet provides a high degree of linearity with high stability for either impulse or steady state signals.

USING THE REACTANCE CHART

[from page 13]

R substituted for $X_{\mathfrak{e}}$ the equation becomes

$$f = \frac{1}{2\pi RC}$$

This equation will be recognized as the equation for the rejection frequency of the parallel-T filter, such as is shown in Fig. 4 providing $C_1 = C_2$ and $R_1 = R_2$ with R_3 and C_3 properly proportioned. This filter is electrically equivalent to the Wein bridge shown in Fig. 5; consequently, the chart may also be used to determine the null frequency of such a bridge, or the frequency of an oscillator employing the Wein bridge for the frequency-determining element.

Thus, it has been shown that the conventional reactance chart may be used without modification for determining component values for the low-pass filter prototype if the values of L and C read from the chart are taken for L/2 and C/2. In the case of the high-pass filter the values indicated by the chart are twice the values given by the filter equations. The value of the series elements of a parallel-T rejection filter or Wein bridge, such as is used frequently in oscillators, are indicated directly on the chart.

Although graphical methods are not recommended for highly accurate work, the results obtained by using the chart are sufficiently accurate for many engineering applications.



MERIT

TRANSFORMERS
Lead Again
or Sound Equipment

for Sound Equipment! with NEW OUTDOOR TYPE

Universal Line Transformers. To couple various line impedances to voice coil. Universal mounting bracket.

Designed specifically for maximum service in the outdoor sound field. Features: Universal mounting (may be bolted er clamped to speaker bracket); Weather-sealed at moderate cost to withstand outdoor cenditions; Encased in one piece drawn metal can; Potted to resist meisture absorption; Terminal board mounted



Mounting JO

Itg. Center Case

23/4 x 37/8

Dimensions H W D

41/4 4-7/16 3-9/16

TYPE	LIST	OHMS IMPEDANCE		
NO.	PRICE	PRIMARY	SEC. W	/ATTS
A-4040	\$ 8.75	250-500-1000-1500-2000	4-8-16	8
A-4041	9.75	250-500-1000-1500-2000	4-8-16	12
A-4042	13:75	250-500-1000-1500-2000	4-8-16	25
A-4043	9.75	45-50	4-8	12

HEAVY DUTY OUTPUT TRANSFORMERS
High Level Type to Couple Line to Speaker
Sec. Impedances: 4-8-15-250-500 Ohms
OPEN MOUNTING D

TYPE NO.	LIST	TUBE	PRI.		PRI. M.A.				
A-3133	\$11.50	P.P. Par. 6L6, P.P. 807	3300	c.t.	240	55			
A-3131	7.00	PP6L6, 6Y6, PP2A3							
		6A3, 6B4, 45, PP6N7	5000	c.t.	80	30			
		46							
A-3128	8.00	PP6V6, 6F6	8000	c.t.	50	14			
*SEALED-IN MOUNTING H									
A-4033	16.50	P.P. Par. 6L6, P.P. 807	3300	c.t.	240	55			
A-4030	13.00	P.P.6L6	6600	c.t.	80	34			
A-4028	12.00	PP6V6, 6F6	8000	c.t.	50	14			
*Wea	therproo	fed, potted for outdoo	r use at	100%	over list pr	ice.			



For information on other transformers see the complete MERIT line in Sam's Red Book or ask for New MERIT Catalog No. 4911



EQUIP WITH MERIT OUTDOOR TYPE TRANSFORMERS TODAY

